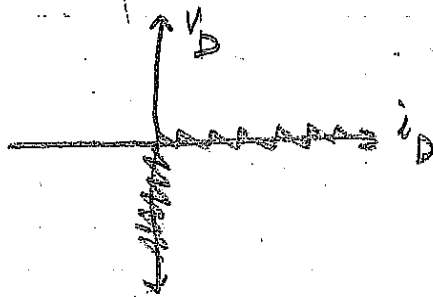
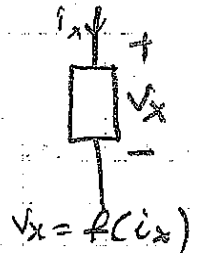


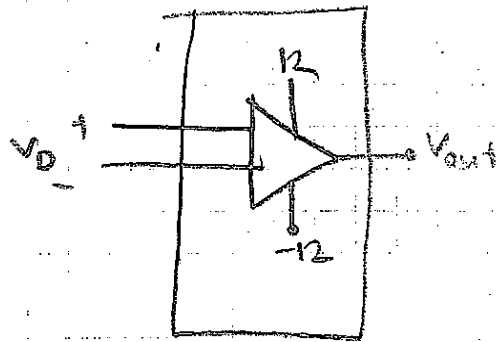
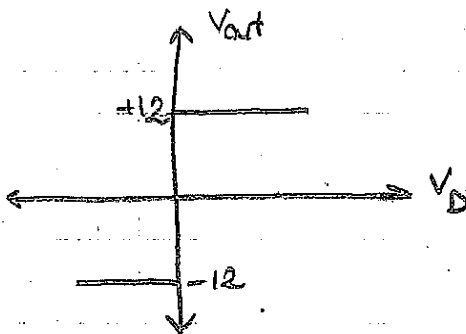
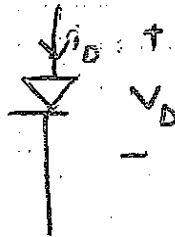
EE 201 Review

Linear Components: $R, L, C \rightarrow$ Terminal equations

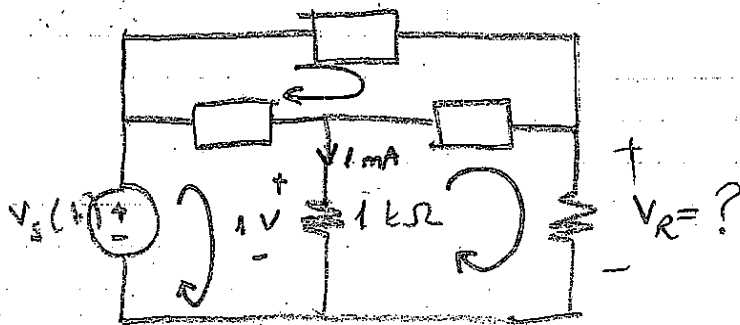
Non-Linear Components:
Diodes, Op-Amp



(i, v) char



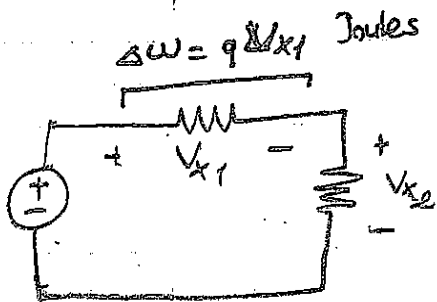
Combination of Components



KVL (\oint Loop) \rightarrow Conservation of energy

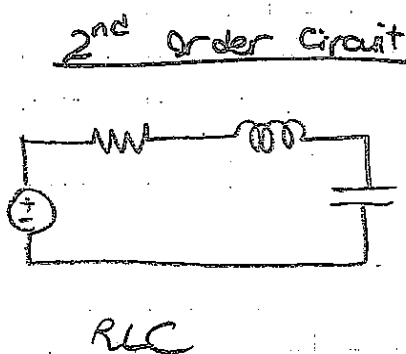
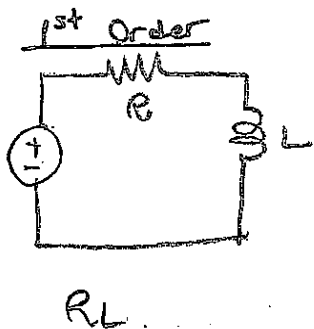
KCL $\sum i_k = 0$ " of charge

$$\sum_{k=1}^{\infty} i_k = 0 \quad (\text{all exiting currents sum to zero})$$



Systematic Analysis Methods

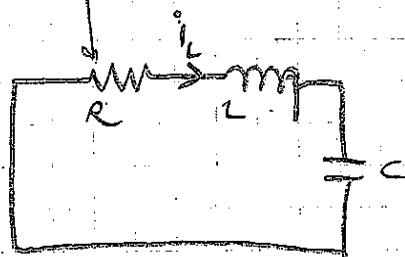
- Node Analysis → (e_A, e_B, e_C) → Node voltage!
- Mesh → (i_1, i_2, i_3) → Mesh currents!
- Thevenin - Norton



- Step Response
- Input Response

zero-state → State: describes "the state" of the circuit
 zero-input Resp.

- RLC → under-damped
 → over-damped
 → critically-damped

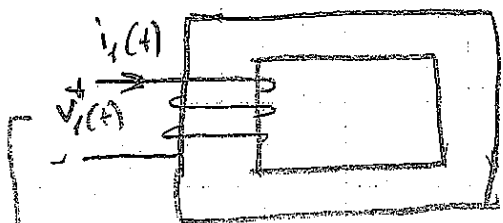


char. eqn: $\lambda^2 + 10\lambda + 20 = 0$

λ : natural freq

$V_C(0^-) = V_0$
 $I_L(0^-) = I_0$

Coupled Inductors



Alternating Current (AC)



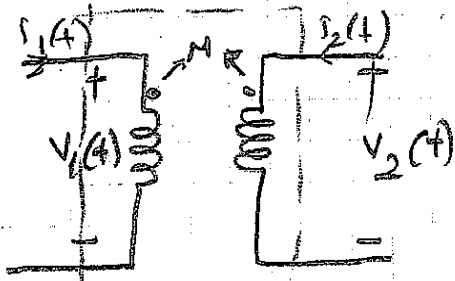
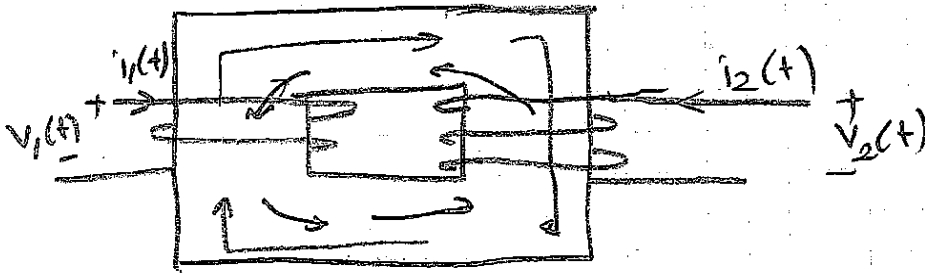
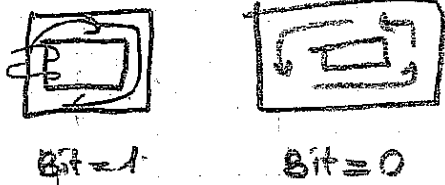
L : Henry (Inductance)

$\phi(t) = L i(t)$

$\left(\frac{d}{dt}\right)$ (Faraday's Law)

$V_L(t) = L \frac{di(t)}{dt}$

Magnetic Memory:



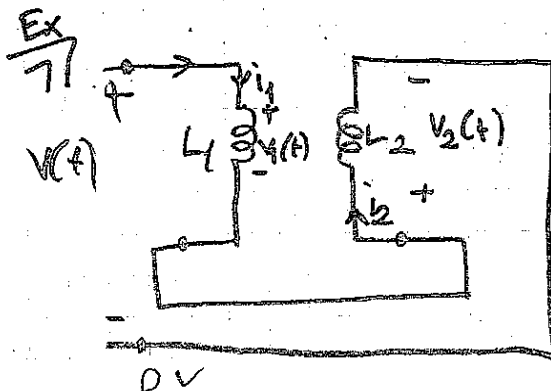
$$\begin{bmatrix} v_1(t) \\ v_2(t) \end{bmatrix} = \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{bmatrix} \frac{d}{dt} i_1(t) \\ \frac{d}{dt} i_2(t) \end{bmatrix}$$

$$\Phi_{tot} = \Phi_1 + \Phi_2$$

$$\Phi_{tot} = L_1 i_1(t) + M i_2(t) \quad \begin{matrix} \text{due to flux coupled} \\ \text{from 2nd winding} \end{matrix}$$

$\frac{d}{dt}$ \downarrow 1st winding

$$v_{L_1}(t) = L_1 \frac{d}{dt} i_1(t) + M \frac{d}{dt} i_2(t)$$



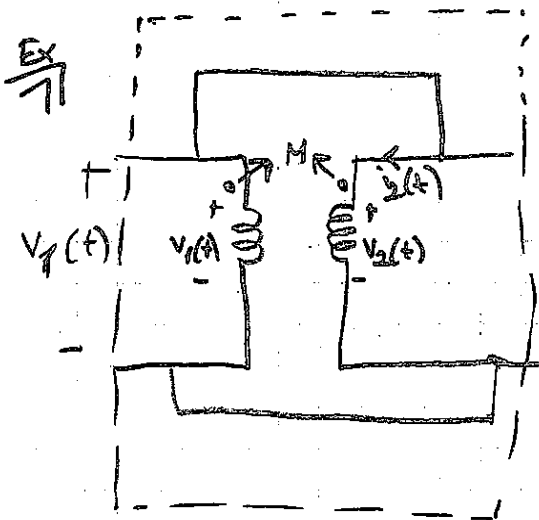
What is the terminal equation of the box?

$$\begin{bmatrix} v_1(t) \\ v_2(t) \end{bmatrix} = \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{bmatrix} \frac{d}{dt} i_1(t) \\ \frac{d}{dt} i_2(t) \end{bmatrix}$$

$$v(t) = v_1(t) + v_2(t)$$

$$v(t) = v_1(t) + v_2(t) = \begin{bmatrix} L_1 + M & L_2 + M \end{bmatrix} \begin{bmatrix} \frac{d}{dt} i_1(t) \\ \frac{d}{dt} i_2(t) \end{bmatrix} \rightarrow i(t)$$

$$v(t) = (L_1 + L_2 + 2M) \frac{d}{dt} i(t)$$



"Parallel configuration"

$$v_1(t) = v_2(t) = v(t)$$

$$i(t) = i_1(t) + i_2(t)$$

$$\begin{bmatrix} v_1(t) \\ v_2(t) \end{bmatrix} = \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{bmatrix} \frac{d}{dt} i_1(t) \\ \frac{d}{dt} i_2(t) \end{bmatrix}$$

$$\frac{d}{dt} \underline{i} = \underline{L}^{-1} \underline{v} \xrightarrow{\text{D}^{-1} \text{ apply}} \underline{i} = \underline{D}^{-1} \underline{L}^{-1} \underline{v}$$

$$\Rightarrow v_1(t) = L_1 \frac{d}{dt} i_1(t) + M \frac{d}{dt} i_2(t)$$

$$\begin{aligned} \text{D}^{-1} v_1(t) &= L_1 i_1(t) + M i_2(t) \\ \text{D}^{-1} v_2(t) &= M i_1(t) + L_2 i_2(t) \end{aligned} = \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

$$\begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix}^{-1} \begin{bmatrix} D^{-1} v_1(t) \\ D^{-1} v_2(t) \end{bmatrix} = \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

Special case for $M=0$

$$\begin{bmatrix} L_1 & 0 \\ 0 & L_2 \end{bmatrix} \begin{bmatrix} D^{-1} v_1(t) \\ D^{-1} v_2(t) \end{bmatrix} = \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

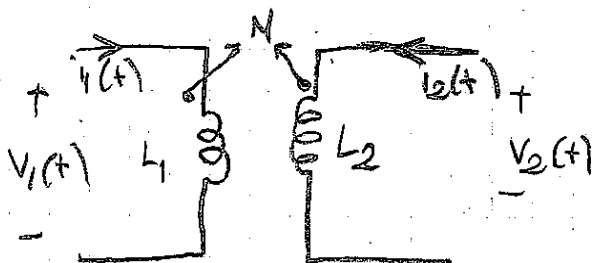
$$\frac{1}{L_1} \int_{-\infty}^t v_1(\tau) d\tau = i_1(t)$$

$$i(t) = i_1(t) + i_2(t) = \Gamma_{11} \int_{-\infty}^t v_1(\tau) d\tau + \Gamma_{12} D^{-1} v_2(t) + \Gamma_{21} D^{-1} v_1(t) + \Gamma_{22} \int_{-\infty}^t v_2(\tau) d\tau$$

$$\begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix}^{-1} = \begin{bmatrix} \Gamma_{11} & \Gamma_{12} \\ \Gamma_{21} & \Gamma_{22} \end{bmatrix} \rightarrow i(t) = (\Gamma_{11} + \Gamma_{12} + \Gamma_{21} + \Gamma_{22}) D^{-1} v(t)$$

$$i(t) = \frac{1}{L_{eq}} D^{-1} v(t)$$

Initial Condition Model for Mutual Inductors



$$i_1(0^-) = I_1$$

$$i_2(0^-) = I_2$$

$$\begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \begin{bmatrix} \frac{d}{dt} i_1(t) \\ \frac{d}{dt} i_2(t) \end{bmatrix}$$

$$\underline{v} = \underline{L} \underline{\dot{i}} + \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

$$D^{-1} \underline{v} = L D^{-1} D \underline{i}$$

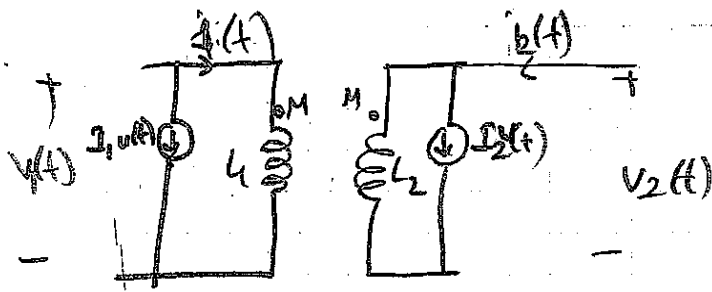
$$\begin{bmatrix} \int_0^+ \frac{d}{dt} v_1(\tau) d\tau \\ \int_0^+ \frac{d}{dt} v_2(\tau) d\tau \end{bmatrix} = \begin{bmatrix} v_1(\tau) \Big|_{\tau=0^-}^{\tau=t} \\ v_2(\tau) \Big|_{\tau=0^-}^{\tau=t} \end{bmatrix} = \begin{bmatrix} v_1(t) - v_1(0^-) \\ v_2(t) - v_2(0^-) \end{bmatrix}$$

$$D^{-1} \begin{bmatrix} v_1(t) \\ v_2(t) \end{bmatrix} = \underbrace{\begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix}}_L \begin{bmatrix} i_1(t) - I_1 \\ i_2(t) - I_2 \end{bmatrix}$$

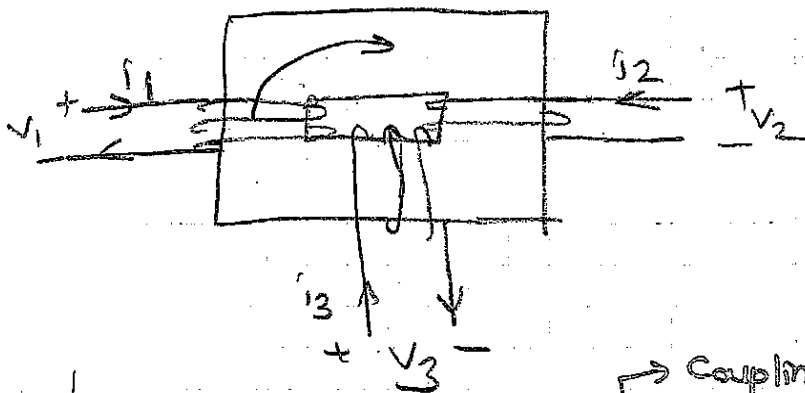
$$L^{-1} \begin{bmatrix} \int_0^+ v_1(\tau) d\tau \\ \int_0^+ v_2(\tau) d\tau \end{bmatrix} = \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix} - \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$$\begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix} = L^{-1} \begin{bmatrix} \int_0^+ v_1(\tau) d\tau \\ \int_0^+ v_2(\tau) d\tau \end{bmatrix} + \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

Special Case: $L^{-1} = \begin{bmatrix} \frac{1}{L_1} & 0 \\ 0 & \frac{1}{L_2} \end{bmatrix}$

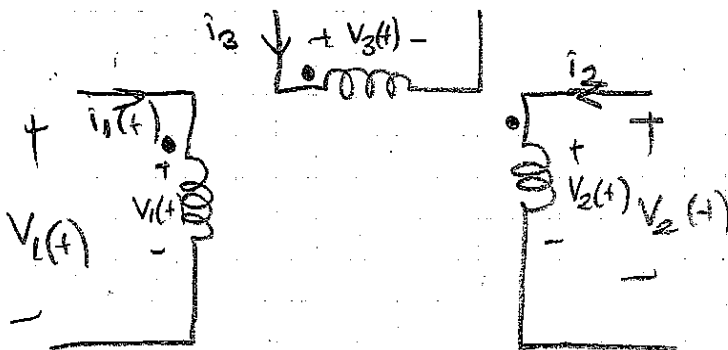


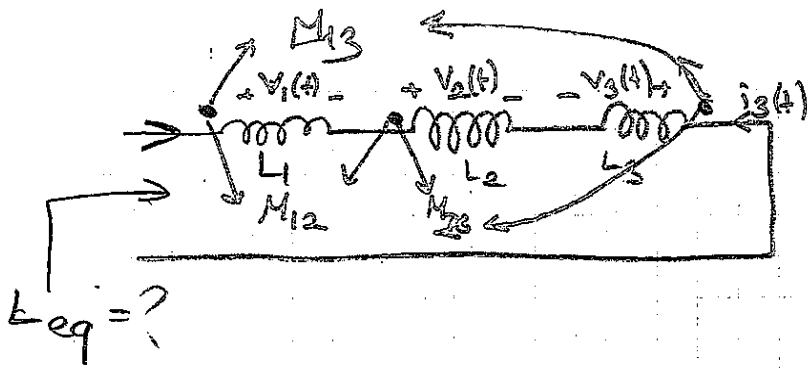
Initial C.M. for mutual ind.



$$\begin{bmatrix} V_1(t) \\ V_2(t) \\ V_3(t) \end{bmatrix} = \underbrace{\begin{bmatrix} L_1 & M_{12} & M_{13} \\ M_{21} & L_2 & M_{23} \\ M_{31} & M_{32} & L_3 \end{bmatrix}}_{\text{Coupling btw 1st \& 2nd winding}} \begin{bmatrix} \frac{di_1(t)}{dt} \\ \frac{di_2(t)}{dt} \\ \frac{di_3(t)}{dt} \end{bmatrix}$$

$$M_{kl} = M_{lk} \rightarrow \underline{\underline{L}} = \underline{\underline{L}}^T \text{ (symmetric)}$$





What is the relation b/w $i(t)$ and $v(t)$ of this component?
(math. reln)

$$v(t) = v_1(t) + v_2(t) - v_3(t)$$

$$= \begin{bmatrix} 1 & 1 & -1 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \\ v_3 \end{bmatrix} = \begin{bmatrix} 1 & 1 & -1 \end{bmatrix} \begin{bmatrix} \frac{d}{dt} i_1(t) \\ \frac{d}{dt} i_2(t) \\ \frac{d}{dt} i_3(t) \end{bmatrix}$$

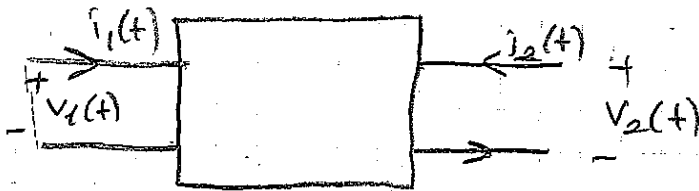
$$= \begin{bmatrix} 1 & 1 & -1 \end{bmatrix} \begin{bmatrix} \frac{d}{dt} i(t) \\ \frac{d}{dt} i(t) \\ -\frac{d}{dt} i(t) \end{bmatrix}$$

$$\begin{bmatrix} L_1 + M_{21} & L_2 + M_{12} & -L_3 + M_{13} \\ -M_{31} & -M_{32} & M_{23} \end{bmatrix} \cdot \begin{bmatrix} v(t) \\ i(t) \\ -i(t) \end{bmatrix}$$

$$v(t) = \left[(L_1 + M_{21} - M_{31}) + (L_2 + M_{12} - M_{32}) + (-L_3 + M_{13} + M_{23}) \right] \frac{d}{dt} i(t)$$

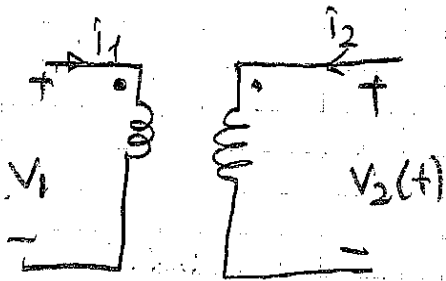
Power

Power & Energy Relations



$$P(t) = v_1(t) i_1(t) + v_2(t) i_2(t)$$

$$= \begin{bmatrix} v_1(t) & v_2(t) \end{bmatrix} \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$



$$P_{mut. ind.}(t) = \begin{bmatrix} v_1(t) & v_2(t) \end{bmatrix} \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

$$= \begin{bmatrix} D_{11} & D_{12} \\ D_{21} & D_{22} \end{bmatrix} \begin{bmatrix} L & M \\ M & L \end{bmatrix} \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

$$P_{mut. ind.} = \begin{bmatrix} \frac{d}{dt} i_1(t) & \frac{d}{dt} i_2(t) \end{bmatrix} \begin{bmatrix} L & M \\ M & L \end{bmatrix} \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

$$= L_1 i_1(t) \frac{d}{dt} i_1(t) + L_2 i_2(t) \frac{d}{dt} i_2(t) + M \left(i_1(t) \frac{d}{dt} i_2(t) + i_2(t) \frac{d}{dt} i_1(t) \right)$$

$\frac{d}{dt} (i_1(t) i_2(t))$
 Watts

Energy: $E = \int_{-\infty}^t P(\tau) d\tau$

\downarrow Joule \downarrow $\frac{\text{Joule}}{\text{sec}} = \text{Watts}$

$$P(t) = \frac{dW(t)}{dt}$$

$$w(t) = \int_{-\infty}^t \left[\frac{d}{dt} i_1(t) \right] \left[\frac{d}{dt} i_2(t) \right] \underline{L} = \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

$$= \frac{1}{2} \begin{bmatrix} i_1(t) & i_2(t) \end{bmatrix} \underline{L} \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix} \Bigg|_{t'=-\infty}^{t'=t}$$

Assuming $i_1(t) = i_2(t) \downarrow_{t=-\infty} = 0$

$$w(t) = \frac{1}{2} \begin{bmatrix} i_1(t) & i_2(t) \end{bmatrix} \underline{L} \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix}$$

$$= \frac{1}{2} \underline{i}^T \begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \underline{i}$$

$$w(t) = \frac{1}{2} L_1 i_1^2(t) + \frac{1}{2} L_2 i_2^2(t) + M i_1(t) i_2(t) \quad \text{Joule}$$

If component is a passive component, $w(t) \geq 0 \quad \forall t$ should be satisfied. Then, for a mutual inductor

$$w(t) \geq 0 \rightarrow \frac{1}{2} \underline{i}^T \underline{L} \underline{i} \geq 0 \quad \forall t \quad (\forall \underline{i} \text{ vectors})$$

\underline{L} : matrices satisfying
 \underline{i}^T satisfying $\underline{i}^T \underline{L} \underline{i} \geq 0$

$\underline{i}^T \underline{L} \underline{i} \geq 0 \rightarrow \forall \underline{i}$ is called positive semi-definite matrix

and $L_{2 \times 2}$ is positive semi-definite

$$\begin{aligned} \text{If } L_1 &> 0 \\ L_2 &> 0 \\ \det(\underline{L}) &> 0 \end{aligned}$$

L : Mutual Inductance Matrix

$L_1 > 0$
 $L_2 > 0$

$\det(\underline{L}) > 0 \rightarrow L_1 L_2 - M^2 > 0$

$\begin{bmatrix} L_1 & M \\ M & L_2 \end{bmatrix} \quad L_1 L_2 - M^2 > 0$

If $L_1 L_2 - M^2 = 0 \xrightarrow{\text{Passive Mut. Ind.}} \det(\underline{L}) = 0 \rightarrow L_1 L_2 - M^2 > 0$

$\frac{M^2}{L_1 L_2} \leq 1$

Coupling coefficient of mutual inductor

$k = \frac{M}{\sqrt{L_1 L_2}}$

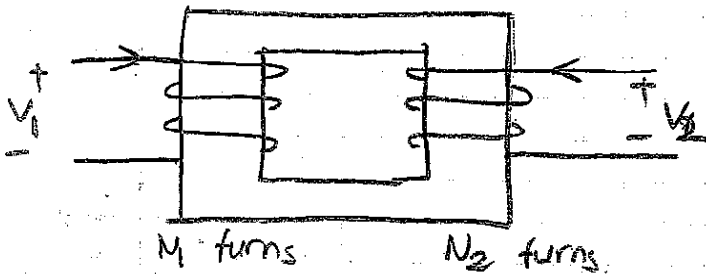
$\rightarrow |k| \leq 1$

$| \text{Coupling coeff.} | \leq 1$

Ideal Transformers

Mutual Inductor with $k=1$ (no ohmic losses)

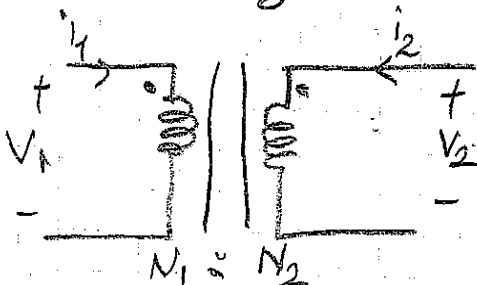
Ideal Transformers



$\frac{V_1}{V_2} = \frac{N_1}{N_2}$ Voltage directly proportional

$\frac{i_1}{i_2} = -\frac{N_2}{N_1}$ Current inversely proportional

Circuit Symbol



N_1 : Turn ratio of primary side

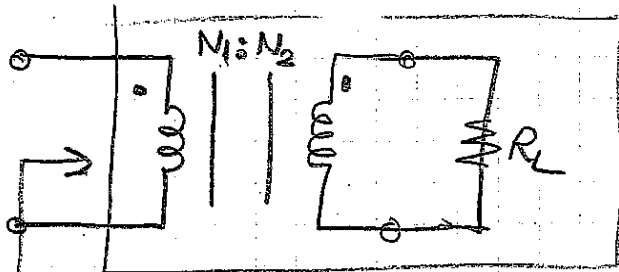
N_2 : " secondary "

$$\begin{aligned}
 P(t) &= \begin{bmatrix} V_1(t) & V_2(t) \end{bmatrix} \begin{bmatrix} i_1(t) \\ i_2(t) \end{bmatrix} \\
 &= V_1(t) i_1(t) + V_2(t) i_2(t) \\
 &= V_1(t) i_1(t) + \left(\frac{N_2}{N_1} V_1(t) \right) \left(-\frac{N_1}{N_2} i_1(t) \right) \\
 &= 0 \quad \forall t
 \end{aligned}$$

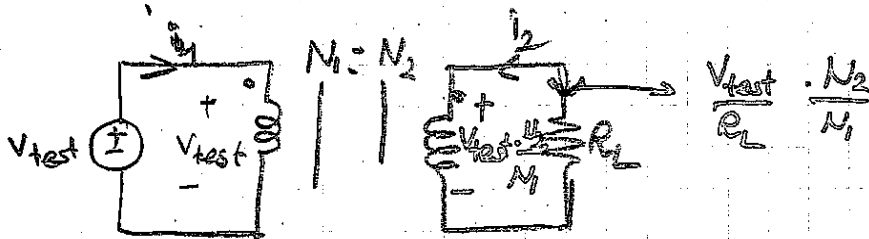
* Ideal transform does NOT absorb/deliver any power at any time

!! Important Property :

Resistance Reflection (Impedance)



$R_{Th} = ?$

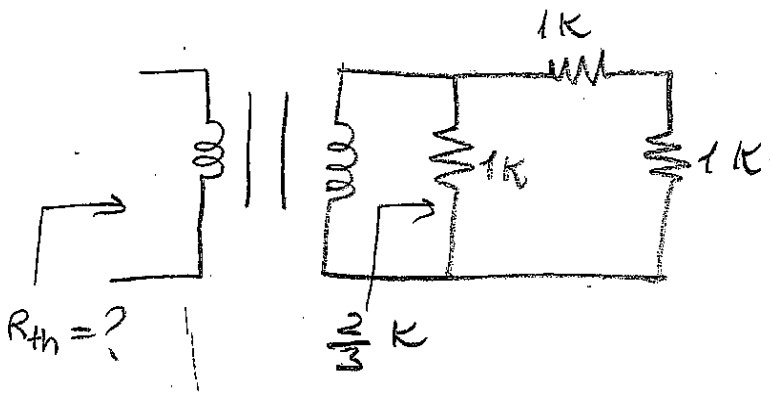


$$R_{Th} = \frac{V_{test}}{I_{test}}$$

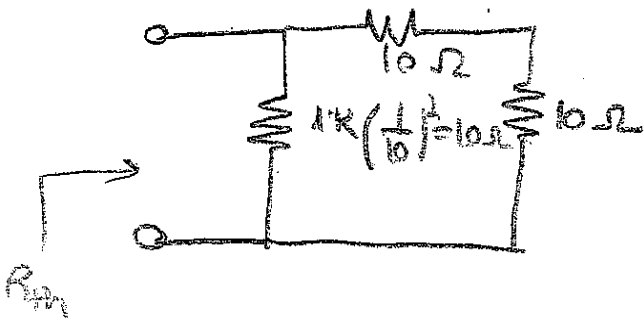
$R_{Th} = \frac{V_{test}}{I_{test}}$
resistance seen from primary side

$$\begin{aligned}
 \frac{V_{test}}{\left(\frac{N_1}{N_2} \right) I_2} &= \frac{V_{test}}{\frac{V_{test}}{R_L} \left(\frac{N_2}{N_1} \right)^2} = \left(\frac{N_1}{N_2} \right)^2 R_L
 \end{aligned}$$

resistance seen from secondary side



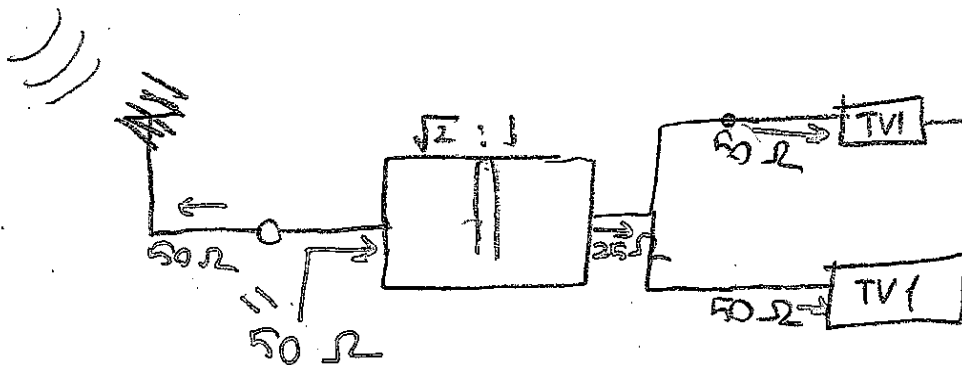
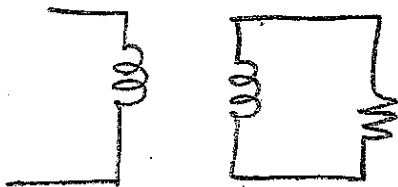
$$R_{Th} = \frac{2}{3} K \cdot \left(\frac{1}{10}\right)^2 = \frac{20}{3} \Omega$$

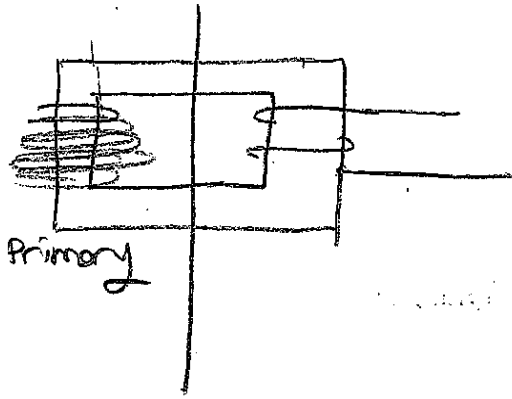
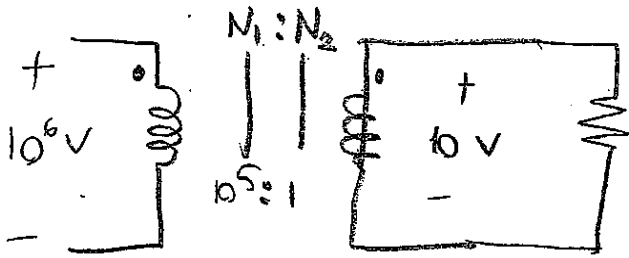


Comment: It is possible to reflect all resistors to the other side

Use of Transformers

1. Impedance / Resistance Matching





Two sides are electrically isolated
(magnetically connected)

3.) Step-Up / Step-Down

Step-Up Voltage increases

Step-Down: " decreases

